Hydrogen – recent and planned research

Burning velocity methane-hydrogen mixtures

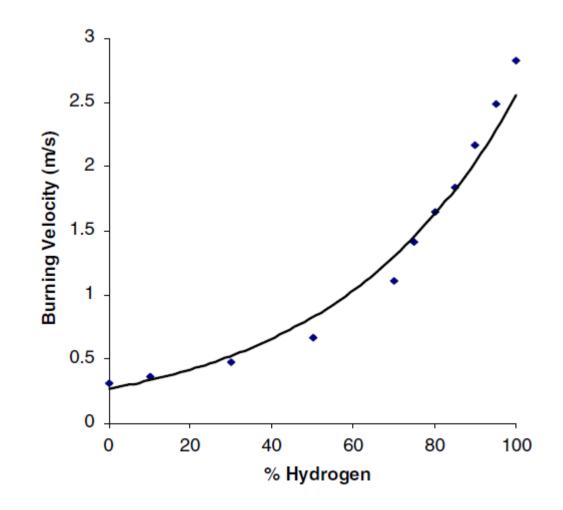


Fig. 16. Burning velocities for different percentage of hydrogen, $\emptyset = 1.0$.

From: Ilbas et al, Laminar-burning velocities of hydrogen-air and

hydrogen-methane-air mixtures: An experimental study, International Journal of Hydrogen Energy 31 (2006) 1768 – 1779

Minimum ignition energy methane-hydrogen mixtures

0.3 Experimental ME $y = 0.2433e^{-0.0221x}$ $R^2 = 0.9507$ △ Reported ME (CH4) 0.2 o Reported ME (H2) ME (m) 0.1 0 100 -25 25 50 75 . 125 Hydrogen percentage in gas mixture (%)

Figure 4.23 : MIE variation for various concentration of hydrogen in mixture

From: Mathurkar, H., Minimum ignition energy and ignition probability for Methane, Hydrogen and their mixtures, PhD Thesis Loughborough University, 2015

Minimum ignition current methane-hydrogen mixtures

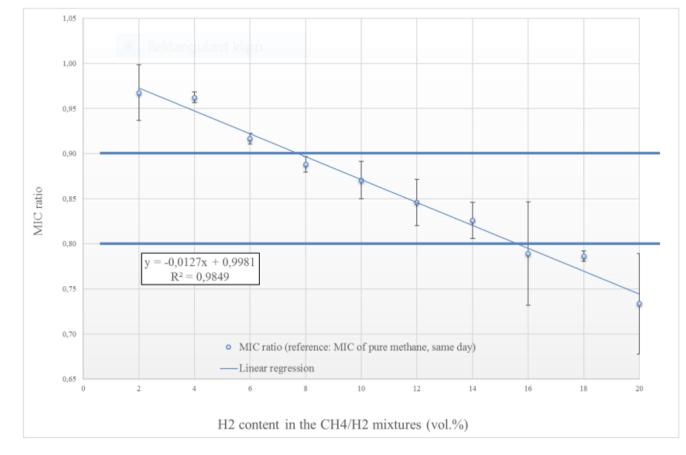


Figure 3: MIC ratio, as a function of hydrogen content in the methane/hydrogen mixtures.

From: Janes et al: Experimental determination of minimum ignition current (mic) for hydrogen /methane mixtures for the determination of the explosion group corresponding to iec 60079-20-1 standard, International conference on hydrogen safety (ICHS 2017), Sep 2017, Hamburg, Germany. pp.54-64.



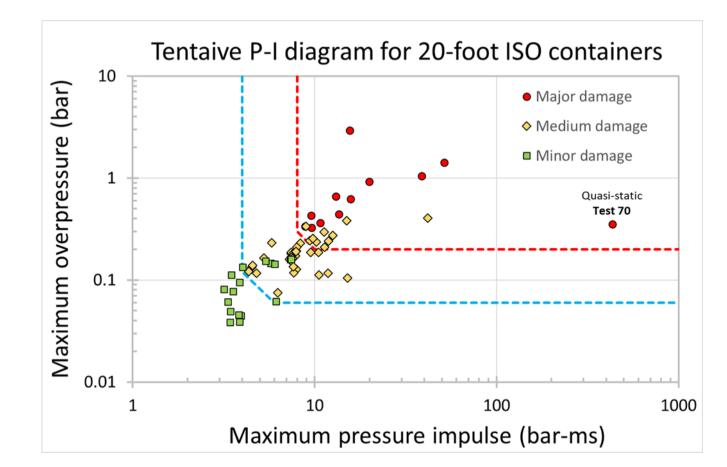
The HySEA project: Main objective

• To conduct pre-normative research on vented hydrogen deflagrations with an aim to provide recommendations for European and international standards on hydrogen explosion venting mitigation systems



Programme of work

- Homogeneous fuel-air mixtures and stratified mixtures
- Blind-prediction exercises
- Consequence assessment



Experimental study on formation and evaporation of LH2 pools (unignited pool)

- Investigation of LH2-pool formation above different substrates,
- Investigation of evaporation rates from LH2-pool above different substrates,
- Investigation of oxygen, nitrogen, moisture carry-over within the pool and the potential for oxygen enrichment in the gas,
- Influence of cross wind conditions using a special ventilation system.



Main findings

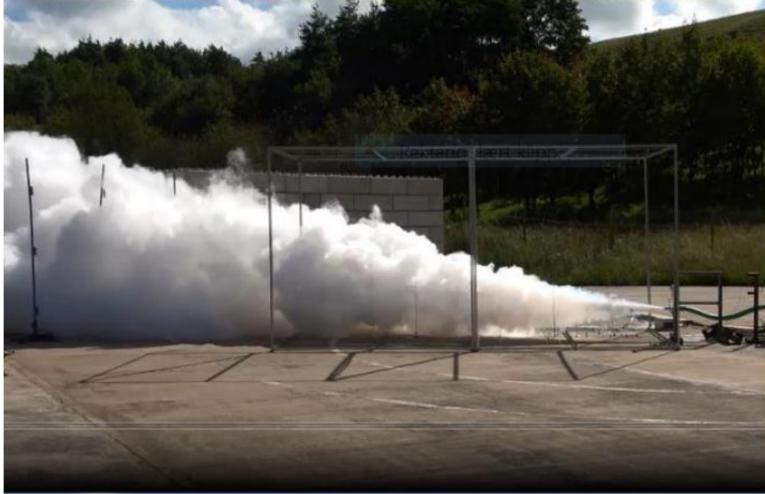
- Data to determine LH2-evaporation rates above different substrates is generated,
- Side wind mainly increases evaporation rate of pool,
- Pools above substrates with low porosity (water, concrete, sand) show quite similar behavior concerning pool formation and evaporation. Evaporation rates mainly governed by material properties of the substrate.
- For gravel pool different behavior was observed, since due to its high porosity (approx. 50% free volume in substrate layer) and the resulting large substrate surface the first pool formation takes much longer and consumes much higher LH2-quantities,
 - When pool evaporation has ended and cold gravel is exposed to ambient air, air components start to condensate/freeze out while the remaining LH2 from within the substrate evaporates,





Rain-out and dispersion from horizontal LH2 releases

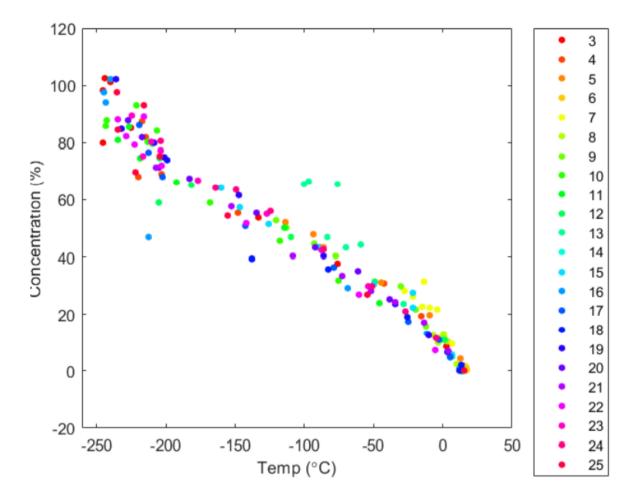
• Mass flow release rates: 100 – 300 g/s



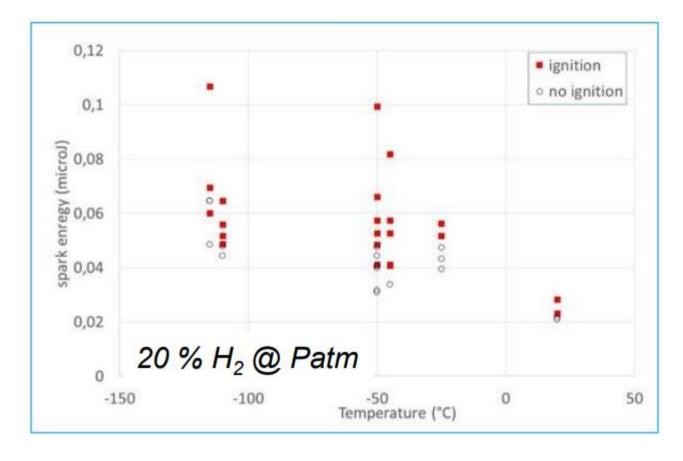


Main findings

- Rainout did not occur during the established flow of these releases
- Pools can form with vertically downwards releases
- Near field dispersion: correlation of concentration with temperature
- Transient ignitable pockets (average H2 concentration > LEL) were measured at 14 m distance from LH2 releases through 12 mm holes or larger
- Following the initial region, approximately 1.5 m for the 1 bar releases and 3 to 6 m for the 5 bar releases, the dispersion of the hydrogen cloud is heavily dependent of the wind, including transient localised gusts



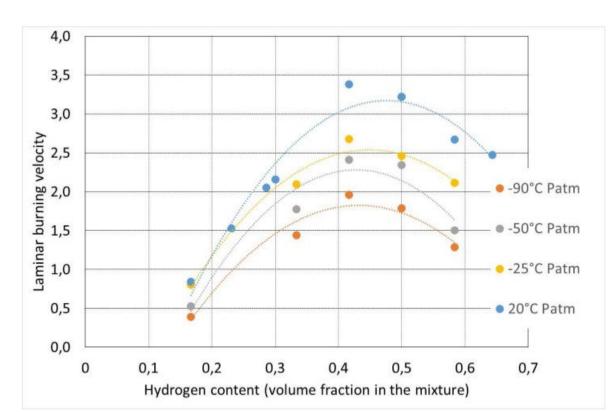
Effect of temperature on explosion properties H2





Temperature (°C)	LFL (% H ₂ v/v)	UFL (% H ₂ v/v)
20	5	70
-60	5.6	66
-120	6	60

Explosion limits

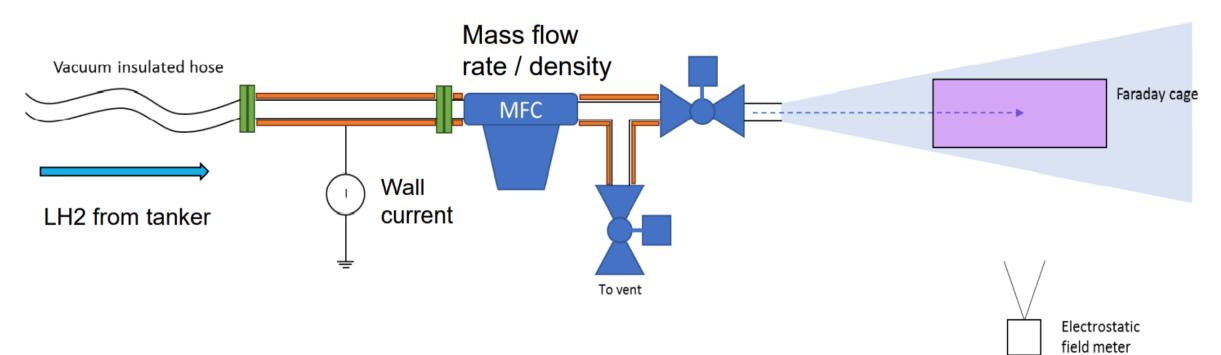


Laminar burning velocity



Electrostatic charge in multiphase hydrogen releases

- Multiphase hydrogen flow can generate a current in pipework especially when two-phase flow occurs
- Occasional spikes in electric field identified in plume of released LH2 (at up to 5 bar) possibly caused by ice breaking off the nozzle or air being ejected from un-purged pipework
- Potential for electrostatic ignition as a result of accidental releases at up to 5 bar appears low providing plant / pipework are earthed.

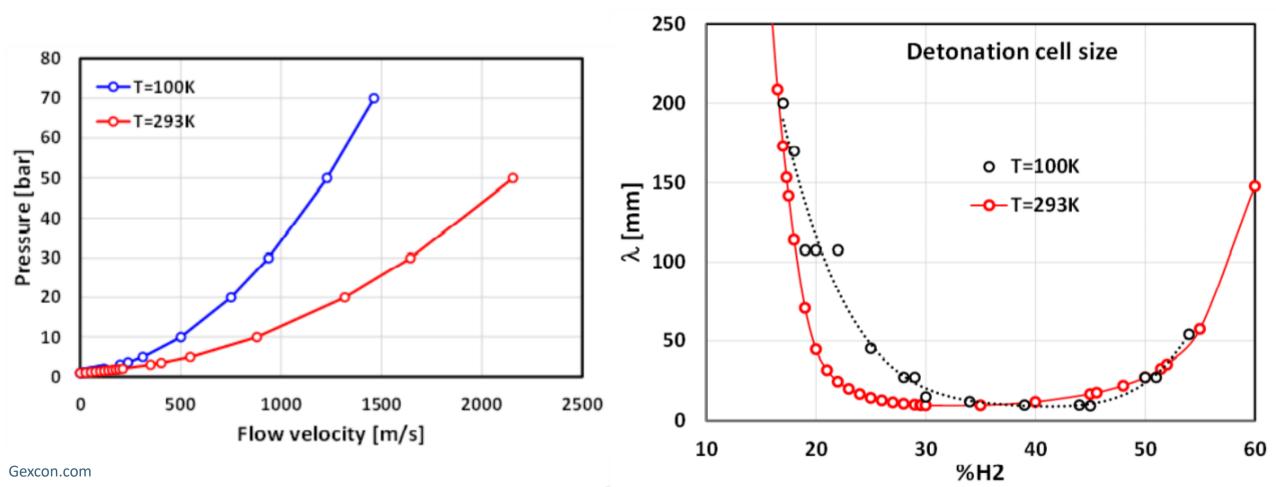




Flame propagation regimes at cryogenic temperature

The run-up distance to detonation at cryogenic temperatures was found to be two times shorter than at ambient temperature.

Measurement of detonation cell sizes



Ongoing research: SH2IFT



- Large-scale experiments to look into the possibility and effects of:
 - BLEVEs of storage vessels containing LH2
 - RPTs when LH2 is released onto or under water



Ongoing research / new opportunities



• Proposal for follow-up of SH2IFT: decision for granting work in course of June

New opportunities

- Tests road tunnel
- Explosion experiments ethylene at high initial pressure and temperature
- Determination MIE Ethylene oxide at high initial pressure and temperature



Application Example

Gexcon.com

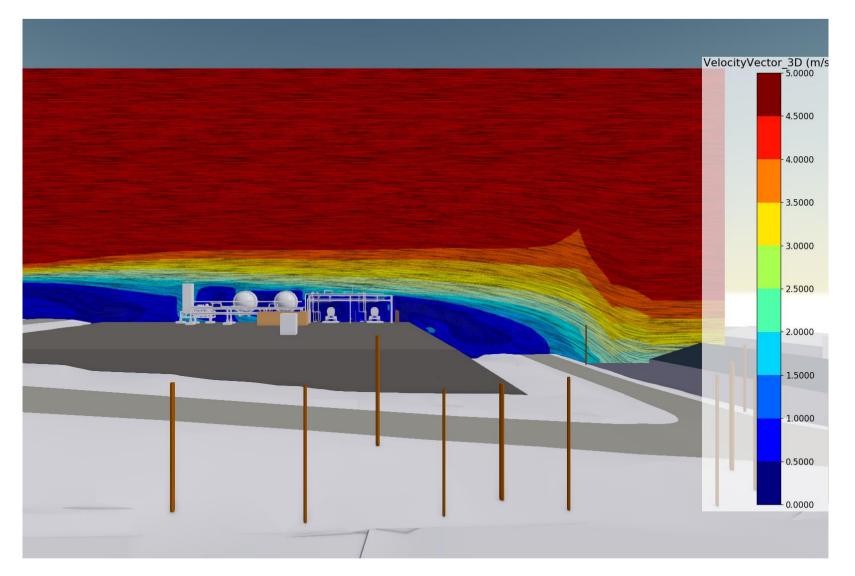
FLACS geometry model

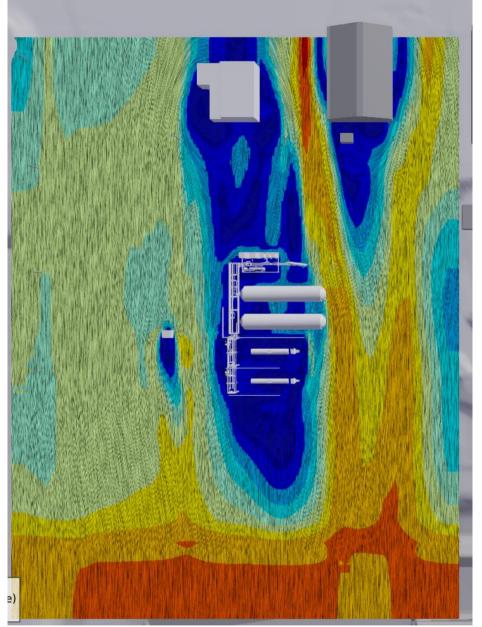
 3D FLACS model generated by Gexcon, landscape and buildings included





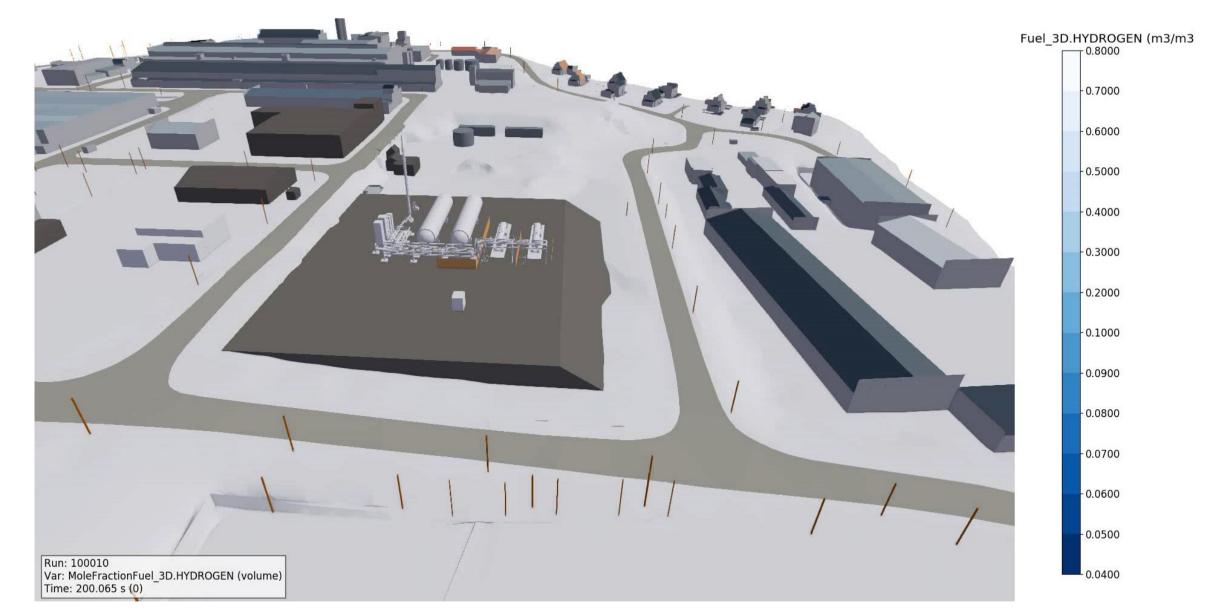
Ventilation Simulations





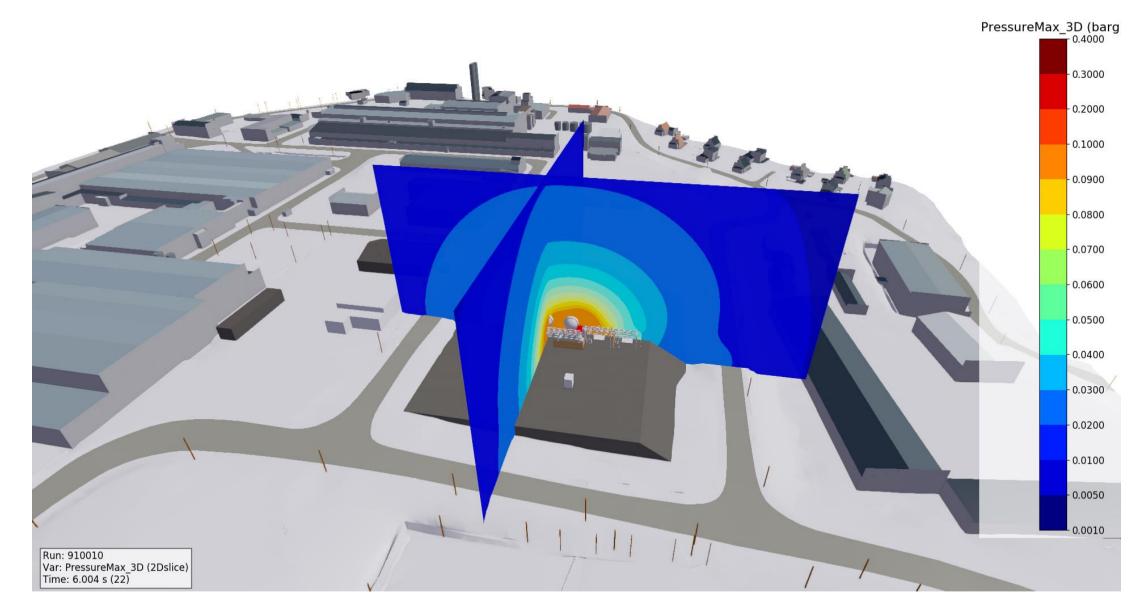


Liquid H2 Dispersion



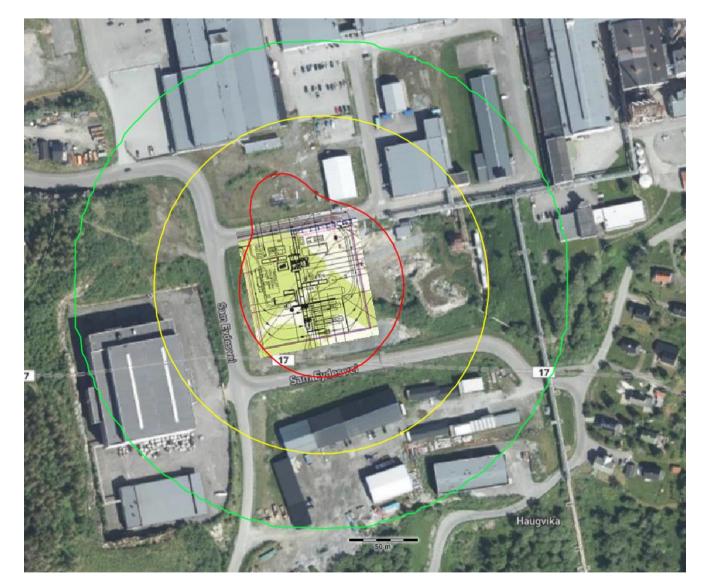


Explosion simulations





Risk Analysis for licensing



- Individual fatality risk contours
- Measurements against numerical risk acceptance criteria



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Thanks for your attention Geirmund Vislie

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